

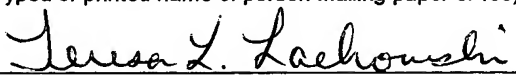
APPLICATION FOR UNITED STATES PATENT

MODIFICATION OF LUBRICANT PROPERTIES
IN AN OPERATING ALL LOSS LUBRICATING SYSTEM

Applicants: Vincent M. Carey
Kevin J. Kelly
Kevin L. Crouthamel
Keith P. Saddler

CROSS-REFERENCE TO RELATED APPLICATION(S):

This application is a Continuation-in-Part of Application Serial No. 10/350,563
filed January 24, 2003.

| | |
|---|----------------------------------|
| "EXPRESS MAIL" mailing label | |
| Number | <u>E U S 6 2 9 0 7 3 4 4 U S</u> |
| Date of Deposit | <u>10/28/03</u> |
| I hereby certify that this paper or fee is being deposited with the United States Postal Service "Express Mail Post Office to Addressee" service under 37 CFR 1.10 on the date indicated above and is addressed to the Commissioner for Patents, P. O. Box 1450, Alexandria, Virginia 22313-1450. | |
| Teresa L. Lachowski | |
| (Typed or printed name of person mailing paper or fee) | |
|  | |
| (Signature of person mailing paper or fee) | |

CASE NO. JJD-0308



27810

PATENT TRADEMARK OFFICE

**MODIFICATION OF LUBRICANT PROPERTIES
IN AN OPERATING ALL LOSS LUBRICATING SYSTEM**

5 **CROSS-REFERENCE TO RELATED APPLICATION(S):**

[0001] This application is a Continuation-in-Part of Application Serial No. 10/350,563 filed January 14, 2003.

10 **Field of Invention**

[0002] The present invention relates generally to the varying of an engine lubricant formulation in response to engine operating conditions. More particularly the invention relates to lubricant components for varying the composition of a marine diesel engine lubricant in response to engine operating
15 conditions.

Background of Invention

[0003] Diesel engines may generally be classified as slow-speed, medium-speed or high-speed engines, with the slow-speed variety being used for the
20 largest, deep draft marine vessels and in industrial applications. Slow-speed diesel engines are typically direct coupled, direct reversing, two-stroke cycle engines operating in the range of about 57 to 250 rpm and usually run on residual fuels. These engines are of crosshead construction with a diaphragm and stuffing boxes separating the power cylinders from the crankcase to prevent
25 combustion products from entering the crankcase and mixing with the crankcase oil. Medium-speed engines typically operate in the range of 250 to about 1100 rpm and may operate on the four-stroke or two-stroke cycle. These engines are trunk piston design, and many operate on residual fuel as well. They may also operate on distillate fuel containing little or no residua. On deep-sea vessels
30 these engines may be used for propulsion, ancillary applications or both. Slow

speed and medium speed marine diesel engines are also extensively used in power plant operations. The present invention is applicable to them as well.

[0004] Each type of diesel engine employs lubricating oils to minimize
5 component wear, remove heat, neutralize and disperse combustion products,
prevent rust and corrosion and prevent sludge formation or deposits. Experience
has shown, however, that no single lubricant formulation can provide optimum
protection against all of the various deleterious conditions to which an engine
may be exposed. Therefore, lubricants typically are formulated to provide at
10 least satisfactory performance for the range of expected engine operating
conditions. For some lubricant applications such as in lubricating cylinders in
crosshead diesel engines that employ all-loss lubrication systems and combust
heavy fuel oil with widely varying sulfur contents, the engine lubrication
requirements vary to such a large degree and with sufficient frequency that one
15 lubricant formulation may not provide adequate performance over the full range
of operating conditions. This inability can result in at least increased engine
maintenance needs and more typically unnecessary expense as a result of repair
costs, down time and excessive oil usage. Thus there is a need for being able to
vary the composition of a lubricant in response to an engine's actual lubrication
20 requirements.

[0005] One object of the invention is to provide lubricant components for real
time varying all-loss, diesel engine's cylinder lubricant properties in accordance
with the engines operating requirements.

25

[0006] Another object of the invention is to provide a low speed diesel engine
oil with improved acid-corrosion protection for operation during conditions
when corrosive wear is high.

[0007] These and other objects will become apparent from the detailed description which follows:

Summary of Invention

5 [0008] Broadly stated, in one aspect the invention includes lubricant components for lubricating a low speed diesel engine cylinder operating under a range of corrosive and abrasive wear operating conditions comprising a primary low speed diesel engine cylinder lubricant and a performance enhancing antiwear and anticorrosive additive selected from the group consisting
10 essentially of (i) an alkylamine-alkylphosphate having at least 1.25 equivalents of alkylamine to 1.0 equivalents of alkylphosphate, (ii) 500 TBN calcium sulfonate, and (iii) mixtures thereof; and means proximate the engine for blending the primary lubricant and additive into a mixture for introduction into the engine when operating conditions require.

15

[0009] In a second aspect, the invention is a method for lubricating the cylinder of a two-stroke, cross-head, marine diesel engine which comprises supplying to the walls of the cylinder a primary low speed diesel engine cylinder lubricant under low wear and corrosion operating conditions and under increased
20 wear and corrosion operating conditions supplying the primary lubricant to the cylinder blended with an antiwear and anti corrosion amount of an additive selected from the above defined group.

[0010] In a third aspect, the invention comprises a method for increasing the
25 TBN of an SAE 50 grade lubricant from about 40 TBN to about 100 TBN without substantially affecting the SAE grade by adding to the lubricant of about 40 TBN a sufficient amount of 500 TBN calcium sulfonate.

Brief Description of Drawing

[0011] The accompanying Figure schematically illustrates a method for practicing the present invention.

5 Detailed Description of Invention

[0012] The lubricating component for lubricating a low speed diesel engine cylinder operating under a range of corrosive and abrasive wear conditions comprise a primary slow speed, two stroke, marine diesel engine lubricant and a performance enhancing antiwear and/or anti corrosive additive.

10

[0013] The primary lubricant comprises a major amount of at least one oil of lubricating viscosity. Thus natural or synthetic oils or mixtures thereof may be used. Natural oils include mineral oils, vegetable oils, solvent treated mineral oils and the like. Synthetic oils include polyalpha olefins, polyol esters, poly
15 internal olefins, polyethylenes, propylenes, polybutenes, polyethyleneglycols, polypropyleneglycols, polyalkyleneglycols, their mixtures and the like, other functional fluids, such as alkylated aromatics, perfluoroalkylpolyethers, polyphenyl ethers, cycloaliphatics, phosphate esters, dialkyl carbonates, silicones, silahydrocarbons, phosphazenes, etc. In general the viscosity of the
20 base oil blend of the primary lubricant herein is in the range of about 5 to about 30 cSt at 100°C.

[0014] The primary lubricant also will include effective amounts of at least one of other additives such as metal detergents, antioxidants, dispersants, pour
25 point depressants, demulsifiers, defoamants, aromatic rich solubilizers, extreme pressure and antiwear additives.

[0015] Useful dispersants include succinimides, succinic acid esters, amides borated succinimides and the like. These typically will be present in an amount

between about 0.10 to about 5.0 wt% based on the total weight of the primary lubricant.

[0016] Suitable metal detergents include calcium and magnesium phenates, sulfonates, salicylates and the like. Typically these will be present from about 0.50 wt% to about 30.0 wt% based on the total weight of the primary lubricant.

[0017] Suitable antioxidants include hindered phenols, arylamines and mixtures thereof. The amount of antioxidants typically will be in the range of 0.1 wt% to 2.0 wt% based on the weight of the primary lubricant.

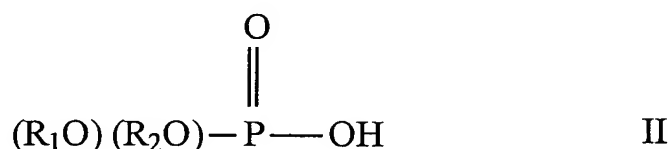
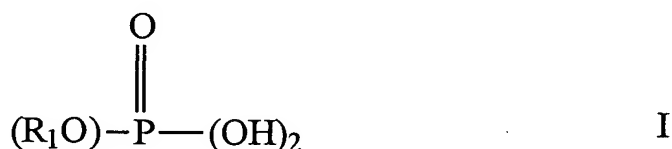
[0018] The aromatic rich solubilizers that are useful in the composition of the invention include alkylated aromatics such as alkylated benzenes, alkylated toluenes, alkylated naphthylenes, alkylated biphenyls and alkylated diphenyl methane. The solubilizer will constitute about 0.20 wt% to about 15.0 wt% of the total primary lubricant.

[0019] Other components that optionally are included in the primary lubricant include anti-foamants, pour point depressants, demulsifiers, extreme pressure agents, antiwear agents, dyes and the like.

[0020] A preferred primary lubricant as a component for use in lubricating a two-stroke, low speed diesel engine cylinder combusting a diesel fuel having from about 0.5 wt% to about 5.0 wt% sulfur, typically will comprise from about 65 wt% to about 90 wt% of a mixture of heavy neutral base oil with a thickening component and from about 10 wt% to about 35 wt% of a combination of the above described additives.

[0021] One suitable antiwear and anti corrosive performance enhancing additive of the lubricant components comprises an alkylamine-alkylphosphate having at least 1.25 equivalents of alkylamine to 1.0 equivalent of alkylphosphate and a nitrogen to phosphorous weight ratio of at least 0.5. In
5 general the ratio, in equivalents of alkylamine to alkylphosphate will range from 1.25:1 to 20:1 and a nitrogen to phosphorous weight ratio of 0.5 to 8 and preferably from 1.5:1 to 5:1 equivalents and a nitrogen to phosphorous weight ratio of 0.6 to 2.

10 [0022] Suitable alkylphosphates are mono and dialkylphosphates and mixtures thereof represented by the formulas I and II:



15 where R_1 and R_2 are the same or different alkyl groups of from about 4 to about 30 carbon atoms and preferably from 6 to 11 carbon atoms. Particularly preferred is a mixture of mono and dialkylphosphates.

20 [0023] Another suitable antiwear and anti corrosive performance enhancing additive of the lubricant components is 500 TBN calcium sulfonate. Indeed 500 TBN calcium sulfonate has been found to be capable of increasing the TBN of

an SAE 50 grade lubricant from about 40 to about 100 without changing the SAE grade of the lubricant.

[0024] Mixtures of the alkylamine-alkylphosphate and calcium sulfonate
5 additives may also be used in the practice of the present invention.

[0025] In the invention mixing and pumping means are provided proximate a
low speed diesel engine for blending the primary lubricant and one or more of
the additives into a mixture and supplying the mixture to the engine when engine
10 operating conditions require.

[0026] The amount of the alkylamine-alkylphosphate additive blended with
the primary lubricant will be a minor, but effective amount, typically ranging
from about 0.05 wt% to about 2.5 wt% based on the total weight of the blended
15 mixture. The amount of the 500 TBN calcium sulfonate additive blended with
the lubricant of about 40 TBN typically will be up to about 15 wt% based on the
total weight of the blended mixture.

[0027] The mixing means employed may be any suitable means such as
20 stirring devices, venturi type devices, static mixers, nozzles and the like.

[0028] The pumping means employed may be any suitable means such as
centrifugal, rotary, fan and displacement type pumps and the like.

25 [0029] Determining when engine operating conditions require supplying the
mixture to the engine may be based, for example, on the operator's experience
and knowledge or on measurement of an actual engine condition parameter, or
measurement of the properties, or condition or both of the cylinder liner scrape-
down oil.

[0030] In one embodiment the primary lubricant is supplied to a low speed diesel engine combusting fuel with lower sulfur levels fuel, e.g., fuel containing about 0.5 to 2.0 wt% sulfur, and the blend is supplied when combusting a higher sulfur level fuel, e.g., fuel containing greater than 2.0 to about 5.0 wt% sulfur.

[0031] In another embodiment an engine condition parameter is measured or predicted from other engine or fuel parameters and blending is performed in response to the measured or predicted parameter.

10

[0032] The invention is now illustrated by reference to the drawing which schematically shows a crosshead diesel engine 1 with a base cylinder oil tank 3 containing a primary lubricant. A second storage tank 5 contains the additive of the present invention. A storage tank 2 for fuel also is provided for supplying fuel to the engine 1 via feed line 4.

15

[0033] The engine lubricant requirements may be directly or predictively measured. For direct measurement, as a non-limiting example, the metal or metal oxide content of the scrape down oil leaving the cylinder (not shown) of engine 1 may be determined. Predictive measurements may include determining the TBN of the scrape down oil, the sulfur content of the fuel, the load on the engine, or the cylinder temperature. Based on the measured or predictive engine parameter the primary lubricant is supplied directly via line 5 to the engine 1 or the primary lubricant is supplied via line 6 to blending means 7 and additive is supplied via line 8 to blending means 7 to generate a mixture which is supplied to engine 1 via line 9.

20

25

[0034] In a preferred embodiment the measured or predictive parameter is entered into a computing device 10 operatively connected to a control device 11.

The computing device 10 is programmed to determine lubricant requirements based on its input and to provide the control device 11 with that determination. The control device 11 is operatively connected to primary lubricant, additive and mixture sources, for example, so as to automatically meter one or all of primary
5 lubricant, additive and mixture as required.

Examples

[0035] The following examples serve to illustrate the invention and its attendant benefits.

10

Example 1

[0036] A commercial marine test engine was operated for 1000 hours using a fully formulated commercial marine oil as a reference for comparison and the same commercial oil to which 0.5 wt% of Mobilad C-423 was added. Mobilad
15 C-423 is a C₁₁-C₁₄ monoalkylamine -C₈ mono and dialkylphosphate additive having 1.75 equivalents of amine per equivalent of phosphates. The cylinder oil feed rate was approximately 25% lower than that used in a typical commercial engine operation thereby placing typical more stress on the cylinder oil. Wear data for cylinder rings and liners was obtained. The results are presented in
20 Table I.

Table I

| | Comparative 1 | Example 1 | % Difference |
|--|---------------|-----------|--------------|
| Average Top Ring Wear Rate, mm/1000 hrs | 0.66 | 0.62 | -6% |
| Maximum Top Ring Wear Rate, mm/1000 hrs | 0.77 | 0.77 | 0% |
| Average Liner Diametral Wear Rate, Full Depth (Subto), mm/1000 hrs | 0.023 | 0.024 | 4% |
| Max. Liner Diametral Wear Rate, Full Depth (Subto), mm/1000 hrs. | 0.134 | 0.126 | -6% |
| Ave. Liner Wear Rate, Top Only (Dimples), mm/1000 hrs. | 0.027 | 0.008 | -70% |
| Max. Liner Radial Wear Rate, mm/1000 hrs | 0.099 | 0.042 | -58% |

Example 2

- 5 [0037] A series of oil compositions were prepared by blending a TBN 40 marine engine oil, oil 1, with different, high TBN additives. The additives used and their amounts are given in Table II. Also given in Table II is the viscosity, the VI, the SAE grade, TBN and storage stability data for each compositions. The storage stability data is obtained by storing the sample at the temperature
- 10 and for the time period given in Table II and when noticeable sediment or floc (suspended particles) appear, measuring the volume percent of such precipitate. In Table II, Tr is trace, F is floc and HF is heavy floc.

Table II

| Description | Comparative 2 Oil 1 | Example 2 Oil 1 + 500 TBN Calcium Sulfonate | Comparative 3 Oil 1 + 300 TBN Calcium Sulfonate | Comparative 4 Oil 1 + 400 TBN Calcium Sulfonate | Comparative 5 Oil 1 + 600 TBN Magnesium Sulfonate | Comparative 6 Oil 1 + 400 TBN Calcium Phenate |
|---|------------------------|---|---|---|--|---|
| Kinetic Viscosity @400°C | 218.2 | 235.5 | 275.2 | 250.2 | 225.6 | 260.3 |
| Kinetic Viscosity @100°C | 19.74 | 21.77 | 24.10 | 22.39 | 20.90 | 22.71 |
| Viscosity Index | 103.4 | 111.1 | 110.4 | 108.9 | 109.8 | 106.9 |
| SAE Grade | 50 | 50 | 60 | 60 | 50 | 60 |
| TBN | 39.7 | 99.3 | 101.6 | 102.1 | 98.6 | 99.2 |
| Storage Stability Room Temp. (Clarity/Vol% Sediment) | | | | | | |
| Initial | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil |
| 1 Day | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil |
| 4 Days | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/2.0 HF | Tr Haze/Nil |
| 15 days | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Hvy/Haze/100 HF | Tr Haze/Nil |
| Storage Stability, 70°C (Clarity/Vol% Sediment) | | | | | | |
| Initial | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil |
| 1 Day | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Hvy Haze/100HF | Tr Haze/Nil |
| 4 Days | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/75 F | Tr Haze/Nil |
| 15 Days | Clear/0.03 | Tr Haze/Nil | Tr Haze/Nil | Tr Haze/Nil | Clear/30 F | Tr Haze/Nil |